

제 11 장

문제 / 풀이

*. $1N = \text{mass } 1\text{kg} \times 1\text{m}/\text{sec}^2 = 10^5 \text{dync}$.
Hz (Hertz) : Unit of frequency (= cycle/sec)

條件. $F_{\max} = 200N$, 진폭 $A_{\max} = 0.1414\text{mm}$

$f_r = 50\text{Hz}$, $f_a = 45\text{Hz}$, $f_b = 55\text{Hz}$

$\eta = \pi (f_b - f_a) = \pi (55 - 45) = \pi \times 10 = 31.42\text{S}^{-1}$
damping coefficient

$A = \frac{A_{\max}}{\sqrt{2}} = \frac{F_0}{2\sqrt{2} \cdot \eta \cdot \omega_n}$ 에서

$m_e = \frac{F_{\max}}{4\pi \cdot A_{\max} \cdot \eta \cdot f_r} = \frac{200}{4\pi \times 0.1414 \times 10^{-3} \times 31.42 \times 50}$
 $= 7.18\text{kg}$.

$$C_d = 2 \cdot M_e \cdot M = 2 \times 7.18 \times 31.42 = 452 \text{ N}\cdot\text{s}/\text{m}$$

$$(*. 1\text{N} = 1\text{kg}\cdot\text{mass} \times 1\text{m}/\text{sec}^2 \rightarrow 1\text{kg}\cdot\text{mass} = \frac{1\text{N}\cdot\text{sec}^2}{\text{m}})$$

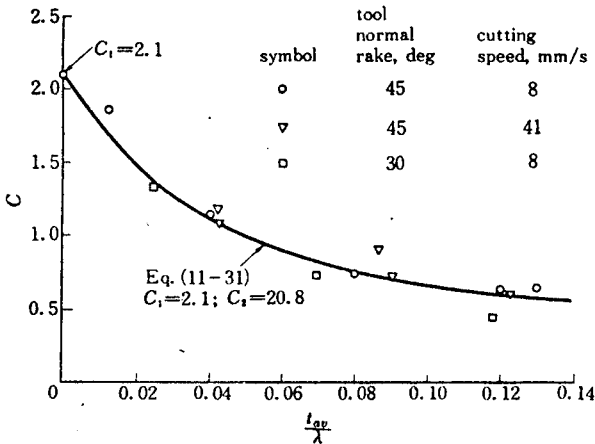
식 (11.23) 에서

$$S_e = \frac{F_{max} \cdot \omega_m^{< 2\pi f_r}}{2 \cdot M \cdot A_{max}} = \frac{F_{max} \cdot 2\pi f_r}{2 \cdot M \cdot A_{max}}$$

$$= \frac{200\text{N} \times 2\pi \times 50}{2 \times 31.42 \times 0.1414\text{mm}} = 7067.42 \text{ N}/\text{mm}$$

[답] · 점성 감쇠 상수 $C_d = 452 \text{ N}\cdot\text{s}/\text{m}$
 · Spring 상수 $S_e = 7067 \text{ N}/\text{mm}$

문제 2 풀이



t_{av} : mean uncut chip thickness, λ : wavelength of work-surface variations. (After Sarnicola and Boothroyd.)

effect of wavelength on the parameter C for a work material of 85/15 brass

안정 조건에서

$$C_d > \frac{b_w \cdot t_{av}}{V} \left[\frac{\tau_s \cdot C}{\theta'} (1 + \cot^2 \phi_{av}) - \tau_s \left(\frac{\sin \alpha_m \{ \cot \phi_{av} + (1+C) \cdot \tan(\alpha_m - \phi_{av}) \} + \cot \alpha_m}{\sin \phi_{av} \cdot \cos(\alpha_m - \phi_{av})} - \theta' \right) \right]$$

그러면 $b_w = 10 \times 10^{-3} \text{ m}$,

$t_{av} = 0.02 \times 10^{-3} \text{ m}$.

$V = 1 \text{ m}/\text{sec}$

$\tau_s = 350 \times 10^6 \text{ N}/\text{m}^2$

$\tau_f = 200 \times 10^6 \text{ N}/\text{m}^2$

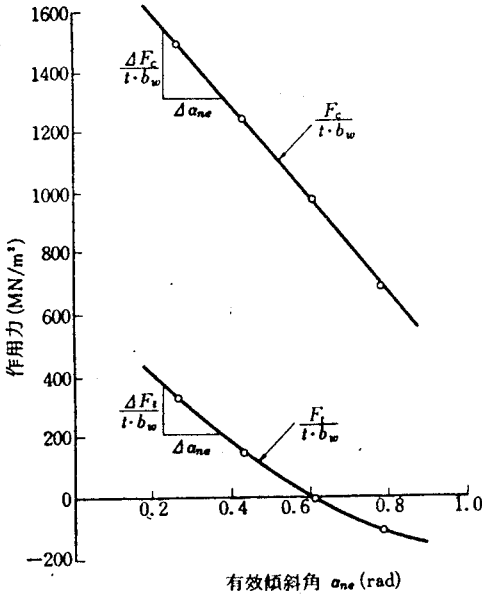
$\phi_{av} = 15^\circ, \alpha_m = 15^\circ (= 0.062 \text{ rad})$

$$\therefore \theta' = \frac{\tau_s}{\tau_f \cdot K} = \frac{\tau_s}{\tau_f} \cdot \frac{t_c}{l_{st}} = \frac{\tau_s}{\tau_f} \cdot \frac{l_{st}}{l_{st}} = \frac{\tau_s}{\tau_f} = \frac{350 \times 10^6}{200 \times 10^6} = 1.75$$

정리에 의하면.

$$\frac{\lambda}{t_{av}} = \frac{V}{f \cdot t_{av}} \quad \text{OK}$$

$$\frac{t_{av}}{\lambda} = t_{av} \cdot \frac{f}{V} = \frac{0.02 \times 10^{-3} \times 50}{1} = 0.001$$



$$\text{Fig 11-15 OK} \Rightarrow C = 2.1$$

$$\text{Fig 11-17 OK}$$

$$\begin{aligned} \sigma_t &= \frac{\Delta F_t}{t \cdot b_w \cdot \Delta \alpha_{ne}} = \frac{\Delta F_t}{t \cdot b_w} / \Delta \alpha_{ne} \\ &= \frac{200 \times 10^6 \text{ N/m}^2}{0.18} = 1.11 \times 10^9 \text{ N/m}^2 \end{aligned}$$

cutting speed : 0.2 m/s, uncut chip thickness : 0.5 mm,
 F_c : cutting force, F_t : thrust, t : uncut chip thickness,
 b_w : width of cut

effect of working normal α_{ne} on cutting forces for a work material of 85/15 brass

$$\begin{aligned} \therefore C_d &> \frac{10 \times 10^3 \times 0.02 \times 10^3}{1} \left\{ \frac{350 \times 10^6 \times 2.1}{1.75} (1 + \cot^2 15^\circ) \right. \\ &\quad \left. - 350 \times 10^6 \left[\frac{\sin 15^\circ \cot 15^\circ + \cos 15^\circ}{\sin 15^\circ} \right] + 1.11 \times 10^9 \right\} \\ &= 924 \text{ N}\cdot\text{s}/\text{m} \end{aligned}$$

[답] 공작재의 상향 칩소형성각의 한

$$C_d = 924 \text{ N}\cdot\text{s}/\text{m}$$